

Analytical and numerical optimization methods for solution of non-smooth dynamic impact problems

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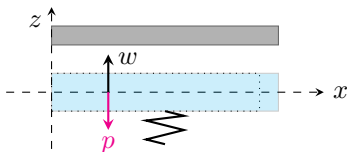
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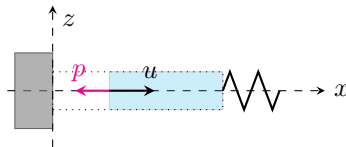


MOTIVATION

- micro (MEMS)/nano (NEMS) electromechanical systems modeled using plates and rods



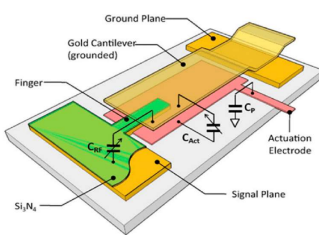
- indentation/ nano-indentation non-destructive testing (NDT) modeled in contact mechanics



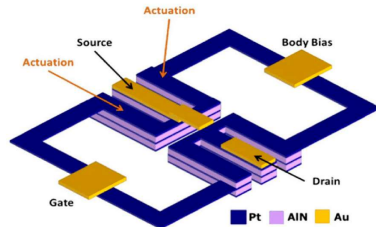
- analytical/ Fourier series solution of dynamic impact problems
- numerical solution with no spurious oscillation, dissipation of energy
- optimal design of flexible structures, distributed sensors and actuators
- inverse problems/ dynamic control for vibration suppression

Sensors and actuators

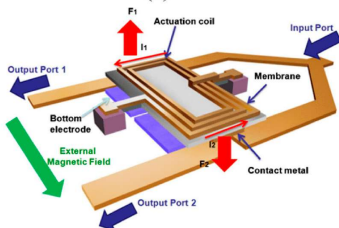
- MEMS-based sensors and actuators



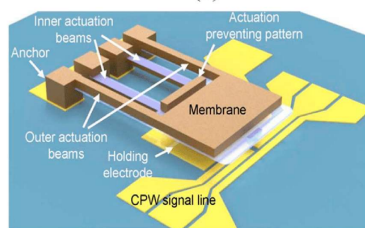
(a)



(b)

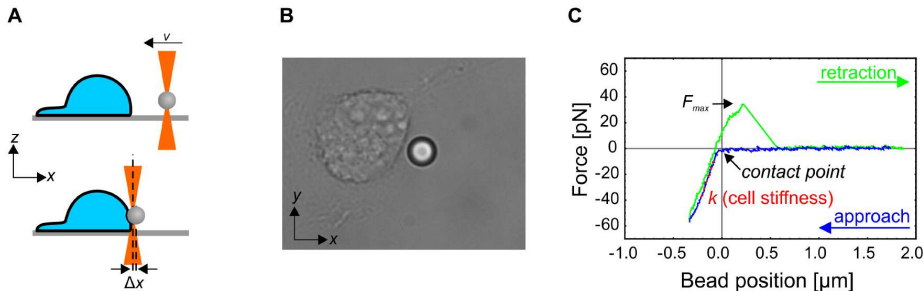


(c)



(d)

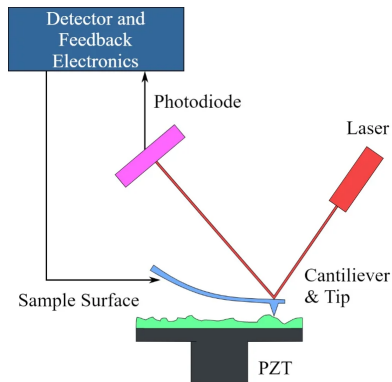
- Cell stiffness measured by lateral indentation



<https://journals.plos.org/plosone/article?id=10.1371/journal.pone.0231606>

- Atomic force microscope

Atomic Force Microscope



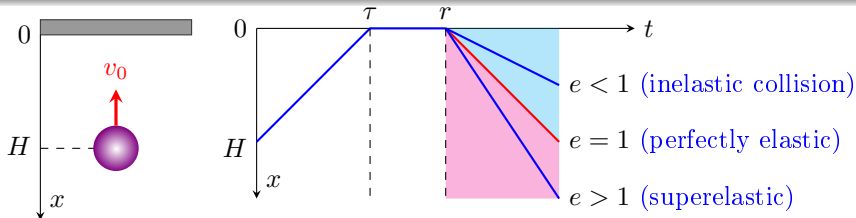
<https://microbenotes.com/atomic-force-microscope-afm/>

OUTLINE

- 1 Motivation
- 2 Impact problems with discontinuous velocity
 - Primal-dual variational formulation
 - Semi-smooth Newton method
 - Space-time (ST) approximation
 - Primal-dual active-set (PDAS) algorithm
- 3 Analytical and numerical solution of 1D benchmark
 - Elastic bar impact against rigid obstacle
 - Bar bouncing in gravity field
 - Control in the oscillating system for vibration reduction
- 4 Conclusion/References

Example of multiple solutions

IMPACT PROBLEMS WITH DISCONTINUOUS VELOCITY



Trajectory $x = u(t)$ of point mass colliding obstacle $x = 0$ at time $\tau = H/v_0$

$$\begin{cases} u_{tt}(t) = \lambda(t), & 0 \leq u(t) \perp \lambda(t) \leq 0 \quad \text{for } t > 0 \\ u(0) = H, & u_t(0) = -v_0 \end{cases}$$

has **multiple solutions** with arbitrary **rebound** time $r \geq \tau$ and speed v_1 :

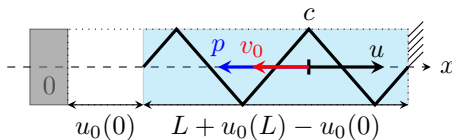
$$\begin{cases} u(t) = -v_0(t - \tau), & \lambda(t) = 0 \quad \text{for } t \in (0, \tau) \\ u(t) = 0, & \lambda(t) = 0 \quad \text{for } t \in (\tau, r) \\ u(t) = v_1(t - r), & \lambda(t) = 0 \quad \text{for } t > r \end{cases}$$

the only **restitution coefficient** $e := \frac{v_1}{v_0} = 1$ at $r = \tau$ **conserves kinetic energy**

Longitudinal impact problem

LONGITUDINAL IMPACT PROBLEM

Elastic bar of length L and wave speed $c = \sqrt{\frac{E}{\rho}}$ colliding rigid obstacle ($x = 0$)



displacement $u(t, x)$, 1D wave equation

$$u_{tt} - c^2 u_{xx} = -p \text{ for } (t, x) \in Q \quad (1)$$

in rectangle $Q := (0, T) \times (0, L)$

under axial deformation $\varepsilon = u_x$ due to either/or/both

- initial deformation $u_0(L) - u_0(0) \neq 0$ (Dirichlet)
- initial speed v_0 (Neumann)
- conservative force p

subject to initial and boundary conditions:

$$\begin{cases} u = u_0, & u_t = -v_0 \text{ as } t = 0 \\ u = 0 \text{ (Dirichlet) or } u_x = 0 \text{ (Neumann) as } x = L \\ 0 \leq u \perp \lambda := c^2 u_x \leq 0 \text{ on } \Gamma := \{x = 0\} \end{cases} \quad (2)$$

Primal-dual variational formulation

- Problem (1)–(2) by **Petrov–Galerkin method**: find solution in **trial space**

$$u - u_0 \in V_{0*} := L^2(0, T; H^1(0, L)) \cap \{v \in H^1(0, T; L^2(0, L)), v(0, \cdot) = 0\}$$

and $\lambda \in L^2(\Gamma)$ validating **primal-dual variational equations**:

$$\begin{cases} 0 \leq u \perp \lambda \leq 0 \text{ on } \Gamma \text{ (} u = 0 \text{ as } x = L \text{ for Dirichlet)} \\ \int_Q (-u_t v_t + c^2 u_x v_x + p v) dx dt + \int_0^L v_0 v|_{t=0} dx = - \int_{\Gamma} \lambda v dt \end{cases} \quad (3)$$

for all functions from **test space** ($v = 0$ as $x = L$ for Dirichlet)

$$v - u \in V_{*0} := L^2(0, T; H^1(0, L)) \cap \{v \in H^1(0, T; L^2(0, L)), v(T, \cdot) = 0\}$$

lack of regularity: $\lambda \in H^{-1/2}(\Gamma)$

- Reducing λ **variational inequality**: find $u - u_0 \in V_{0*}$ such that $u \geq 0$ on Γ

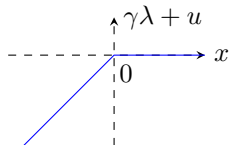
$$\int_Q (-u_t (v_t - u_t) + c^2 u_x (v_x - u_x) + p(v - u)) dx dt + \int_0^L v_0 (v|_{t=0} - u_0) dx \geq 0$$

for all test functions $v - u \in V_{*0}$ such that $v \geq 0$ on Γ

Semi-smooth Newton method

Complementarity conditions can be expressed by **merit function**

$$0 \leq u \perp \lambda \leq 0 \iff M(z) = 0, \quad z := (u, \lambda)$$



for arbitrary constant $\gamma > 0$ **min-based** merit function

$$M(z) := \min(u, -\gamma\lambda) = \min(\gamma\lambda + u, 0) - \gamma\lambda$$

which is **non-smooth** at $z = 0$

$$\begin{cases} M'_u(z) = 1, & M'_\lambda(z) = 0 & \text{if } \gamma\lambda + u < 0 \\ M'_u(z) = 0, & M'_\lambda(z) = -\gamma & \text{if } \gamma\lambda + u \geq 0 \end{cases}$$

M has the **generalized derivative** in **finite dimensions**:

$$\|M(z^\star + h) - M(z^\star) - (M'_u, M'_\lambda)(z^\star + h) \cdot h\|_{\mathbb{R}^N} = \mathcal{O}(\|h\|_{\mathbb{R}^N})$$

and in **infinite dimensional spaces with gap** $1 \leq p < q$:¹

$$\|M(z^\star + h) - M(z^\star) - (M'_u, M'_\lambda)(z^\star + h) \cdot h\|_{L^p} = \mathcal{O}(\|h\|_{L^q})$$

¹M. Hintermüller, K. Ito, K. Kunisch, The primal-dual active set strategy as a semismooth Newton method, *SIAM J. Optimiz.* **13** (2006) 865–888

Space-time (ST) approximation

SPACE-TIME (ST) APPROXIMATION

- Piece-wise polynomials on triangular meshes $\mathcal{T}_h$ in **space-time FE** space

$$V^h := \{v_h \in C(\overline{Q}), v_h \in \mathbb{P}_1(K) \text{ for } K \in \mathcal{T}_h\} \subset H^1(Q)$$

its trial and test function sub-spaces ($v_h = 0$ as $x = L$ for Dirichlet):

$$V_{0*}^h := \{v_h \in V^h, v_h(0, \cdot) = 0\}, \quad V_{*0}^h := \{v_h \in V^h, v_h(T, \cdot) = 0\}$$

spanned by **nodal basis** $\{\phi_h\}$ and ϕ_m at $t_m = mh$, $h = \frac{T}{M}$ on $\Gamma = \cup_{m=1}^M T_m$

- Approximate (3) using **primal-dual active/inactive set** formalism

$$\left\{ \begin{array}{l} u_h = 0 \text{ on } \mathcal{A}_h := \{\cup T_m : \gamma\lambda_m + \frac{1}{2}(u_h(t_{m-1}, 0) + u_h(t_m, 0)) < 0\} \\ \lambda_h = 0 \text{ on } \mathcal{I}_h := \{\cup \overline{T}_m : \gamma\lambda_m + \frac{1}{2}(u_h(t_{m-1}, 0) + u_h(t_m, 0)) \geq 0\} \\ r_m := \int_Q (-u_{ht}\phi_{mt} + c^2 u_{hx}\phi_{mx} + p\phi_m) dxdt + \int_0^L v_0\phi_m\delta_{m0} dx \\ \quad = \frac{1}{2}(\lambda_m + \lambda_{m+1})h \quad \text{for } m = 0, \dots, M-1 \\ \int_Q (-u_{ht}\phi_{ht} + c^2 u_{hx}\phi_{hx} + p\phi_h) dxdt = - \int_0^L v_0\phi_h|_{t=0} dx \quad \forall \phi_h \neq \phi_m \end{array} \right. \quad (4)$$

for hyperbolic equations, **no M-property, even no P-property!**

ST-PDAS algorithm

Space-time primal-dual active-set (ST-PDAS) algorithm

- 1:** Initialize $\mathcal{A}_h^0 = \emptyset$ and $\mathcal{I}_h^0 = [0, T]$; set iteration number $k = 0$
2: Find solution $u_h^k - u_{0h} \in V_{0*}^h$ to the **linear system**

$$\begin{cases} u_h^k = 0 & \text{on } \mathcal{A}_h^k, & u_{hx}^k = 0 & \text{on } \mathcal{I}_h^k \\ \int_Q (-u_{ht}\phi_{ht} + c^2 u_{hx}\phi_{hx} + p\phi_h) dxdt + \int_0^L v_0\phi_h|_{t=0} dx = 0 \end{cases}$$

for all basis functions $\phi_h \in V_{*0}^h$ with $\phi_h = 0$ on Γ

- 3:** Determine **residuals** $r_h^k = \{r_m^k\}$ and **multipliers** $\lambda_h^k = \{\lambda_m^k\}$ from recursion

$$\begin{cases} r_m^k = \int_Q (-u_{ht}\phi_{mt} + c^2 u_{mx}\phi_{hx} + g\phi_m) dxdt - \int_0^L v_0\phi_m\delta_{m0} dx \\ \lambda_0^k := 0, & \lambda_{m+1}^k = \frac{2}{h}r_m^k - \lambda_m^k & \text{for } m = 0, \dots, M-1 \end{cases}$$

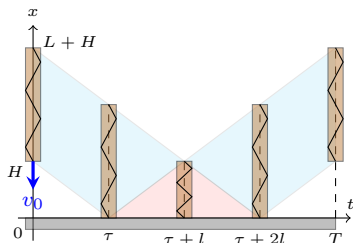
- 4:** Update **active/inactive sets**

$$\begin{cases} \mathcal{A}_h^{k+1} = \{\cup T_m : \gamma\lambda_m^k + \frac{1}{2}(u_h^k(t_{m-1}, 0) + u_h^k(t_m, 0)) < \text{tol}\}, \\ \mathcal{I}_h^{k+1} = \{\cup \bar{T}_m : \gamma\lambda_m^k + \frac{1}{2}(u_h^k(t_{m-1}, 0) + u_h^k(t_m, 0)) \geq \text{tol}\} \end{cases}$$

- 5:** If $\mathcal{A}_h^{k+1} = \mathcal{A}_h^k$ or cycling then **STOP**; else set $k = k + 1$ and go to **2**

Elastic bar impact against rigid obstacle

ANALYTICAL AND NUMERICAL SOLUTION OF 1D BENCHMARK



bar initial speed v_0 , length L , height H
 impact time $\tau := \frac{H}{v_0}$, $l := \frac{L}{c}$, wave speed c

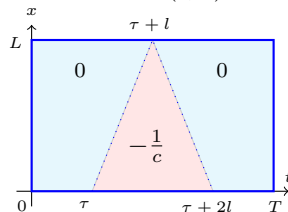
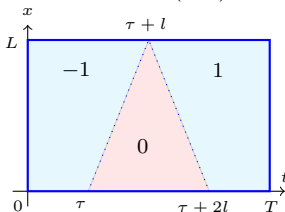
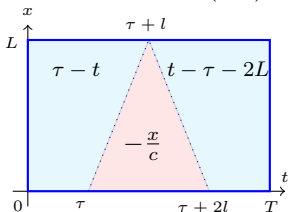
$$\begin{cases} u_{tt} - c^2 u_{xx} = 0 & \text{in } Q = (0, T) \times (0, L) \\ u = H, \quad u_t = -v_0 & \text{as } t = 0 \\ u_x = 0 & \text{as } x = L \\ 0 \leq u \perp \lambda = c^2 u_x \leq 0 & \text{as } x = 0 \end{cases}$$

bar position $x + u(t, x)$, analytical piece-wise linear solution for $v_0 < c$:

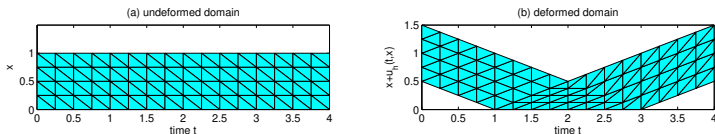
displacement $u(t, x) : v_0$

velocity $u_t(t, x) : v_0$

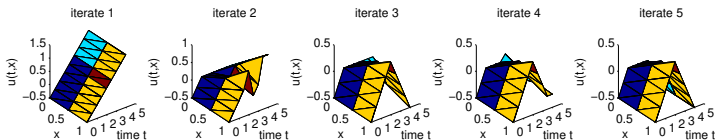
strain $u_x(t, x) : v_0$



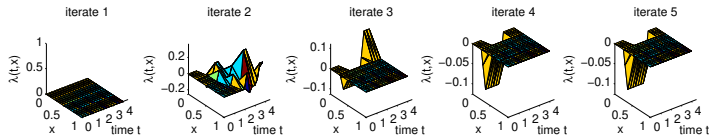
ST-PDAS solution as $c = 1$, $L = 1$, $H = \frac{1}{2}$, $v_0 = \frac{1}{2}$



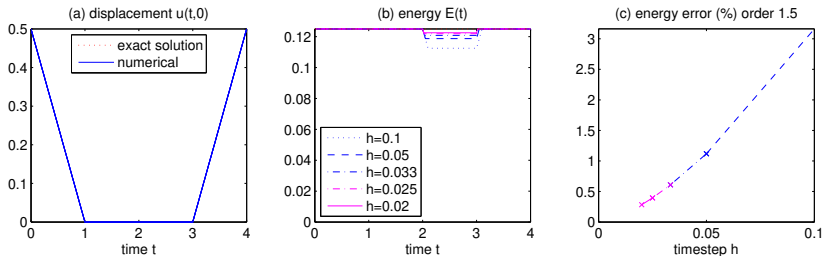
ST-PDAS numerical iterates of displacement $u_h(t, x)$:



contact force $c^2 u_{hx}(t, x)$ implying multiplier λ_h on Γ as $x = 0$:



ST-PDAS convergence over uniform triangular mesh

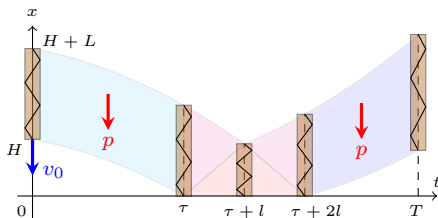


features of **ST-PDAS solution**:

- algorithm converges in **few iterates**
- **numerical and exact solutions** coincide on nodes ($\sim 10^{-14}$)
- solution has **no oscillation**
- energy has **no dissipation**
- speed of convergence is **super-linear**

Bar bouncing in gravity field

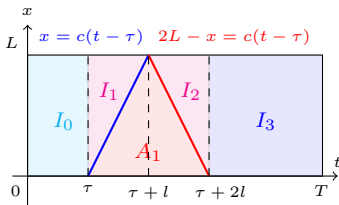
BAR BOUNCING IN GRAVITY FIELD



field p , impact time $\tau := \frac{\sqrt{v_0^2 + 2pH} - v_0}{p}$

$$\begin{cases} u_{tt} - c^2 u_{xx} = -p & \text{in } (0, T) \times (0, L) \\ u = H, \quad u_t = -v_0 & \text{as } t = 0 \\ u_x = 0 & \text{as } x = L \\ 0 \leq u \perp \lambda = c^2 u_x \leq 0 & \text{as } x = 0 \end{cases}$$

bar position $x + u(t, x)$, generalized D'Alembert formula $u(t, x) =$



if $v_0 + p\tau = \sqrt{v_0^2 + 2pH} \geq 2pl$

$$\begin{cases} H - v_0 t - \frac{p}{2} t^2 = (\tau - t)(v_0 + \frac{p}{2}(\tau + t)) & \text{in } I_0 \\ (\tau - t)(v_0 + p\tau) + p\eta(t, x) & \text{in } I_1 \\ -(v_0 + p\tau)\frac{x}{c} + p\eta(t, x) & \text{in } A_1 \\ (v_0 + p\tau)(t - \tau - 2l) + p\eta(t, x) & \text{in } I_2 \\ (v_0 + p\tau)(t - \tau - 2l) - \frac{p}{2}(t - \tau - 2l)^2 & \\ + p\chi(t, x) & \text{in } I_3, \quad \lambda(t) = \begin{cases} -c(v_0 + pt) & \text{on } A_1 \\ 0 & \text{else on } \Gamma \setminus A_1 \end{cases} \end{cases}$$

Vibrations

- double Fourier series for **clamped bar vibrations** of period 4π

$$\eta(t, x) := \frac{2}{Lc^2} \sum_{n=1}^{\infty} \frac{(\cos \nu_n c(t-\tau) - 1) \sin \nu_n x}{\nu_n^3}, \quad \nu_n := \frac{\pi}{L} \left(n - \frac{1}{2}\right)$$

$$\begin{cases} \eta_{tt} - c^2 \eta_{xx} = -\frac{2}{L} \sum_{n=1}^{\infty} \frac{\sin \nu_n x}{\nu_n} = -1 \text{ as } t \in \mathbb{R}, x = L \\ \eta = 0, \quad \eta_x = -\frac{2}{Lc^2} \sum_{n=1}^{\infty} \frac{\cos \nu_n c(t-\tau) - 1}{\nu_n^2} = \frac{t-\tau}{c} \text{ as } x = 0 \\ \eta = 0, \quad \eta_t = 0 \text{ as } t = \tau; \quad \eta_x = 0 \text{ as } x = L \end{cases}$$

- double Fourier series for **free bar vibrations** of period 2π

$$\chi(t, x) := \frac{4}{c^2} \sum_{n=1}^{\infty} \frac{\cos \mu_n (c(t-\tau) - 2L) \cos \mu_n x}{\mu_n^2} - \frac{2L^2}{3c^2}, \quad \mu_n := \frac{\pi n}{L}$$

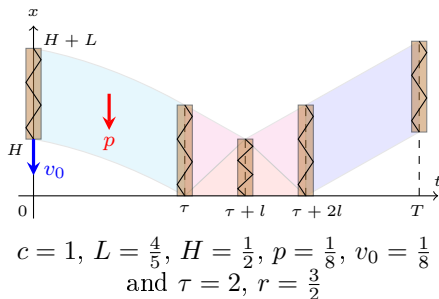
$$\begin{cases} \chi_{tt} - c^2 \chi_{xx} = 0 \text{ as } t \in \mathbb{R}, x \in (0, L) \\ \chi = \frac{x^2 - L^2}{c^2}, \quad \chi_t = 0 \text{ as } t = \tau + 2l; \quad \chi_x = 0 \text{ as } x = 0, L \\ \chi = (t - \tau - (2k+1)l)^2 - l^2 \text{ for } t - \tau \in 2l(k, k+1) \text{ as } x = 0 \quad (k \in \mathbb{N}) \end{cases}$$

Control in the oscillating system for vibration reduction

CONTROL IN THE OSCILLATING SYSTEM FOR VIBRATION REDUCTION

Under step-wise loading

$$p(t) = \begin{cases} p & \text{for } t \in (0, \tau) \\ 0 & \text{for } t \in (\tau, T) \end{cases}$$

non-oscillatory solution to the impact problem given analytically $u(t, x) =$ 

$$\begin{cases} H - v_0 t - \frac{p}{2} t^2 & \text{in } I_0 \\ (\tau - t)(v_0 + p\tau) & \text{in } I_1 \\ -(v_0 + p\tau) \frac{x}{c} & \text{in } A_1 \\ (v_0 + p\tau)(t - \tau - 2l) & \text{in } I_2 \cup I_3 \end{cases}$$

$$\lambda(t) = \begin{cases} -c(v_0 + p\tau) & \text{on } A_1 \\ 0 & \text{else on } \Gamma \setminus A_1 \end{cases}$$

CONCLUSION

- Motivation stemming from elastodynamic contact problems with **non-smooth velocities**, which are stated in a weak variational form
- Implementing by **space-time (ST)** finite-element approximation and **primal-dual active set (PDAS)** method of semi-smooth Newton type
- 1D benchmark modeling and constructing **explicit solutions** for axial impact of an elastic bar against a rigid obstacle
- Numerical ST-PDAS experiments on uniform triangulations yielding **high accuracy, no oscillation, no dissipation, super-linear convergence**
- **Inverse problems** to control oscillations and suppress vibrations
- Challenging **2D/3D analysis**

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